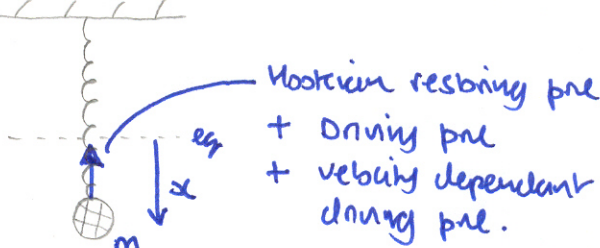


WAVES

Single, Driven, Damped 1D oscillator



General equation for linear damping

pre: $F_{\text{damp}} \propto -\dot{x}$ is:

$$\ddot{x} + 2\gamma\dot{x} + \omega_0^2 x = f(t) \quad (*)$$

Notes: γ is a damping coefficient
 $\frac{\omega_0}{2\pi}$ is frequency of oscillations when $f(t)=0$, $f(t) = \text{Driving force}/m$
 $\gamma=0$.

LINEAR 2nd order differential equation. (Ordinary).

Hence general solution is solution to $\ddot{x} + 2\gamma\dot{x} + \omega_0^2 x = 0$ + function usually similar to $f(t)$ that satisfies (*). i.e., $x(t) = CF + PI$. Note CF will have 2 arbitrary constants determinable by b.c.'s. i.e., $x(0) = \text{constant}$, $\dot{x}(0) = \text{constant}$.

Now interesting case occurs when $f(t) = \text{Re}(F e^{i\omega t})$ [$m = \text{oscillator mass}$] known.
 For convenience write $x(t) = \text{Re}(z(t)) \Rightarrow (*)$ becomes:

$$\ddot{z} + 2\gamma\dot{z} + \omega_0^2 z = \frac{F}{m} e^{i\omega t}$$

Now CF (= TRANSIENT solution)

takes form $e^{-\delta t} (A e^{i\omega_1 t} + B e^{-i\omega_1 t})$ with $\omega_1^2 = \omega_0^2 - \gamma^2$

PI (= STEADY STATE) takes form $C e^{i\omega t}$ which by substitution yields:

$$C = \frac{F}{m} \left\{ \frac{(\omega_0^2 - \omega^2) - 2i\gamma\omega}{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2} \right\}$$

since $e^{-\delta t}$ prefix will cause transients to die / decay with time steady state becomes most important

in steady state $\text{Re}(z(t)) = x(t) = |C| \cos(\omega t + \arg(C))$ in the long term.

So $|C|$, the steady state amplitude demonstrates the forced response of the oscillator. $|C|$ as a function of ω will demonstrate RESONANCE, i.e. a peak at some value of ω . (Usually close to ω_0).

Note, since $z = C e^{i\omega t}$ in steady state, velocity response, characterised by $\dot{z} = i\omega C e^{i\omega t}$ will also exhibit resonant behaviour. Note phase change with z of $\pi/2$.

Now define IMPEDANCE ($|Z|$) as $\left| \frac{\text{Force}}{\text{velocity}} \right|$ which in above case

$$|Z| = \left| \frac{F e^{i\omega t}}{i\omega C e^{i\omega t}} \right| = \left| \frac{F}{\omega C} \right|$$

This clearly will exhibit resonant behaviour as well.

Not so useful in this case but very handy when considering waves or boundaries and more generally.

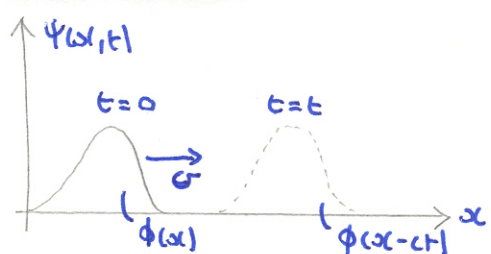
Other definitions (Applicable to (*)).

QUALITY FACTOR: $Q = \frac{\omega_0}{2\gamma}$ - used to characterise oscillation

[For $f(t)=0$, $Q = \text{number of cycles the oscillator goes through for the energy to fall by } 1/e$; 2π times the energy stored in the system / energy lost per cycle]

INSTANTANEOUS POWER: $P = \text{Re}(F e^{i\omega t}) \text{Re}(\dot{z})$ MEAN POWER = $\frac{1}{2} \text{Re}(F \omega^* C)$

The wave equation - consider a function $\phi(x)$ propagating at velocity v in the x direction s.t. its profile does not change.



i.e., $\phi(x,t) = \phi(x-ct)$ let $u = x-ct$

$\Rightarrow \phi(x,t) = \phi(u)$. By chain rule: $\frac{\partial \phi}{\partial x} = \frac{d\phi}{du} \frac{\partial u}{\partial x} = \frac{d\phi}{du} \Rightarrow \frac{\partial^2 \phi}{\partial x^2} = \frac{d^2 \phi}{du^2} \frac{\partial u}{\partial x} = \frac{d^2 \phi}{du^2}$

Similarly: $\frac{\partial^2 \phi}{\partial t^2} = v^2 \frac{d^2 \phi}{du^2} \Rightarrow$ 1D wave equation:

$\frac{\partial^2 \phi}{\partial x^2} = \frac{1}{v^2} \frac{\partial^2 \phi}{\partial t^2}$

which generalises in 3D to $\nabla^2 \phi = \frac{1}{v^2} \frac{\partial^2 \phi}{\partial t^2}$

Note LINEAR EQUATION - g. solution $f(x-ct) + g(x+ct)$.

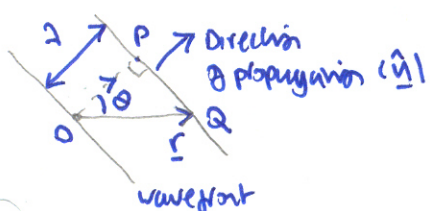
Plane and Spherical Harmonic waves

In above example $\phi(x)$ is shifted by ct in x direction via transform of $x \rightarrow x-ct$. For a time function i.e., $e^{i\omega t}$, same propagation can be explained by a time transform of $t \rightarrow t - \frac{x}{v}$ i.e., $\phi(x,t) = Ae^{i\omega(t - \frac{x}{v})} \Rightarrow \phi(x,t) = Ae^{i(\omega t - kx)}$

with k being ω/v . Note ωt and kx are non dimensional angles or PHASES. kx altered by 2π when $x = \lambda$ (wavelength) so $k = \frac{2\pi}{\lambda}$

Similarly $\omega T = 2\pi \Rightarrow \omega = 2\pi f$ (T = period, f = frequency) so as $k = \frac{\omega}{v}$

$\Rightarrow v \cdot \frac{2\pi}{\lambda} = 2\pi f \Rightarrow v = f\lambda$. Note per convention a 1D wave (travelling) is written as $\phi(x,t) = Ae^{i(kx - \omega t)}$ for +ve x propagation. For a 3D plane wave:



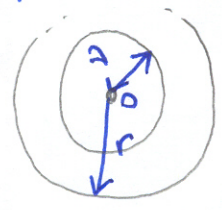
* $P \rightarrow Q$ line has same phase relative to O .
 * phase at $P = k \cdot r \cos \theta = \underline{k} \cdot \underline{r}$ defining wave vector \underline{k} as $k \hat{n} = \frac{2\pi}{\lambda} \hat{n}$.

Hence $\phi(\underline{r}, t) = Ae^{i(\underline{k} \cdot \underline{r} - \omega t)}$ for a plane wave.

For a spherical wave: since wave energy $\propto |\phi|^2$, and energy flow across a sphere of radius $r \propto 4\pi r^2 |\phi|^2$; assuming no losses:

$4\pi r^2 |\phi|^2 = \text{constant} \Rightarrow \phi \propto \frac{1}{r}$ Hence for spherical wave:

$\phi(r,t) = \frac{A}{r} e^{i(kr - \omega t)}$



assume θ is small

Waves (transverse) on a taut string - similar method used for ELASTIC WAVES

let ϕ be displacement (transversely) of a uniformly taut string under tension T .

\Rightarrow regarding piece on segment Δx (in ϕ direction), if string has mass/unit length ρ by Newton's 2nd law:

$\rho \Delta x \frac{\partial^2 \phi}{\partial t^2} = T \sin(\theta + \Delta\theta) - T \sin \theta \approx T \cos \theta (\theta + \Delta\theta) - T \cos \theta \theta$

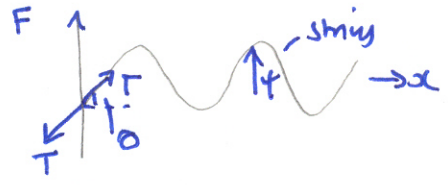
Now $\cos \theta \approx \frac{\partial \phi}{\partial x}$ and $\cos(\theta + \Delta\theta) \approx \frac{\partial \phi}{\partial x} + \frac{\partial}{\partial x} \left(\frac{\partial \phi}{\partial x} \right) \Delta x = \frac{\partial \phi}{\partial x} + \frac{\partial^2 \phi}{\partial x^2} \Delta x$

so $\rho \Delta x \frac{\partial^2 \phi}{\partial t^2} = T \frac{\partial^2 \phi}{\partial x^2} \Delta x$ i.e., wave equation, $v = \sqrt{\frac{T}{\rho}}$

More waves on a string To produce a transverse travelling wave must

apply driving force which balances the transverse component of string tension at the point of driving.

i.e. driving force = $F = -T \sin \theta \approx -T \tan \theta \approx -T \frac{\partial \phi}{\partial x}$

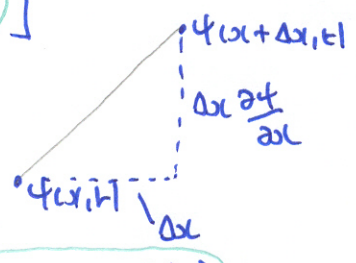


So 'impedance' of string = $\left| \frac{F_{\text{osc}}}{v_{\text{velocity}}} \right|$
 $= \left| \frac{-T \frac{\partial \phi}{\partial x}}{\frac{\partial \phi}{\partial t}} \right|$ Now $\phi(x,t) = \phi(x \pm vt)$

$z_{\text{string}} = \frac{T}{v} = \sqrt{T \rho} = \rho v$

[Note: for elastic waves: Pressure waves have $z_p = \left| \frac{\tau_{xx}}{u_x} \right| = \left| \frac{M_c \frac{\partial u_x}{\partial x}}{\frac{\partial u_x}{\partial t}} \right| = \sqrt{M_c \rho}$
 Shear waves have $z_s = \left| \frac{\tau_{xy}}{u_x} \right| = \left| \frac{\mu \frac{\partial u_x}{\partial y}}{\frac{\partial u_x}{\partial t}} \right| = \sqrt{\mu \rho}$

Now for waves on a string: work done on segment Δx in passing of wave (= PE density $\times \Delta x$)
 = T. extension = $T \left\{ (\Delta x^2 + (\Delta x \frac{\partial \phi}{\partial x})^2)^{1/2} - \Delta x \right\}$



$\approx \frac{T}{2} \left(\frac{\partial \phi}{\partial x} \right)^2 \Delta x$ (expanding binomially) \Rightarrow PE density = $\frac{T}{2} \left(\frac{\partial \phi}{\partial x} \right)^2$

Now KE density = $\frac{1}{2} \rho \left(\frac{\partial \phi}{\partial t} \right)^2$ But since $\phi(x,t) = \phi(x \pm vt)$, $\left(\frac{\partial \phi}{\partial t} \right)^2 = v^2 \left(\frac{\partial \phi}{\partial x} \right)^2$
 [use $u = x \pm ct$ and chain rule] \Rightarrow PE density = $\frac{T}{2} \cdot \frac{1}{v^2} \left(\frac{\partial \phi}{\partial t} \right)^2$ Now $v^2 = \frac{T}{\rho}$

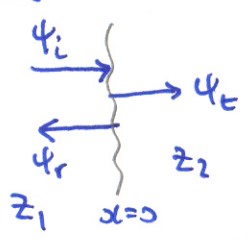
So PE density = $\frac{\rho}{2} \left(\frac{\partial \phi}{\partial t} \right)^2$ i.e. PE density = KE density. So TOTAL

energy density = PE + KE = $\rho \left(\frac{\partial \phi}{\partial t} \right)^2$ For harmonic wave $\phi(x,t) = A e^{i(kx - \omega t)}$
 $\langle \text{energy density} \rangle = \rho \langle \left(\frac{\partial \phi}{\partial t} \right)^2 \rangle = \rho \langle -i \omega A e^{i(kx - \omega t)} \rangle^2 = \frac{1}{2} \rho \omega^2 A^2$

so after time Δt , extra length $v \Delta t$ is oscillating so average wave power input = $\frac{1}{2} \rho \omega^2 A^2 v \Delta t / \Delta t = \frac{1}{2} \rho \omega^2 A^2 v = \frac{1}{2} z \omega^2 A^2$

These results are GENERAL wave phenomena / properties.

Reflection and Transmission of INCIDENT PLANE WAVES on a boundary



consider boundary separating two media of impedances z_1, z_2 .
 Boundary conditions are: ϕ continuous and $\frac{\partial \phi}{\partial x}$ continuous.
 (i.e. no 'kinks' and joint transverse force = $-T \frac{\partial \phi}{\partial x}$)
 $\Rightarrow \omega$ is constant but since $z = \frac{T}{v} \Rightarrow k, v$ must vary.

let $\phi_i = I e^{i(k_1 x - \omega t)}$ $\phi_r = R e^{i(-k_1 x - \omega t)}$ $\phi_t = T e^{i(k_2 x - \omega t)}$ so applying b.c's

at $x=0$: ① $I + R = T$ ② $k_1 I - k_1 R = k_2 T$ Now $k = \frac{\omega}{v}$

so ②: $I \frac{1}{v_1} - R \frac{1}{v_1} = T \frac{1}{v_2}$ Now $\frac{T}{v}$ ($T = \text{Tension}$) = z so since T must be

constant: $\Rightarrow z_1 I - z_1 R = z_2 T$ ③ Now $z_2 \text{ ①} - \text{②} \Rightarrow I(z_1 + z_2) + R(z_2 + z_1) = 0$

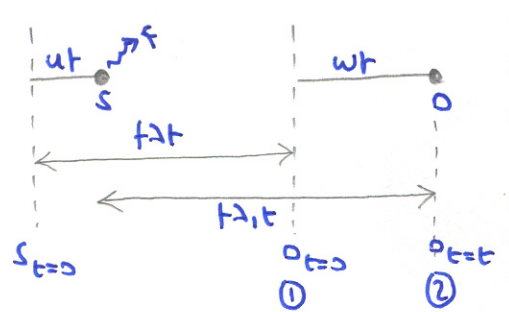
$\Rightarrow \frac{R}{I} = \frac{z_1 - z_2}{z_1 + z_2}$, and $z_1 \text{ ①} + \text{②} \Rightarrow 2z_1 I = T(z_1 + z_2) \Rightarrow \frac{T}{I} = \frac{2z_1}{z_1 + z_2}$
 $\frac{R}{I}$ and $\frac{T}{I}$ are REFLECTION COEFFICIENTS.

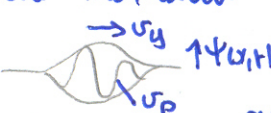
Reflection and Transmission of energy - Power of Harmonic wave (Average) = $\frac{1}{2} Z \omega^2 A^2$
 (A = 141). \therefore on our boundary: energy input = $\frac{1}{2} Z_1 \omega^2 I^2$, reflection = $\frac{1}{2} Z_1 \omega^2 R^2$, transmission = $\frac{1}{2} Z_2 \omega^2 T^2$
 \Rightarrow $\frac{\text{reflected energy}}{\text{incident energy}} = \frac{Z_1}{Z_2} \frac{R^2}{I^2} = \left(\frac{Z_1 - Z_2}{Z_1 + Z_2} \right)^2$; $\frac{\text{transmitted}}{\text{incident}} = \frac{Z_2}{Z_1} \frac{T^2}{I^2} = \frac{4Z_1 Z_2}{(Z_1 + Z_2)^2}$

Note $Z = \left| \frac{\text{Force}}{\text{velocity}} \right|$ is not always real and Z (i.e. in EM) can be COMPLEX. In this case replace above by $\left| \frac{Z_1 - Z_2}{Z_1 + Z_2} \right|^2$ and $1 - \left| \frac{Z_1 - Z_2}{Z_1 + Z_2} \right|^2$ since $\left| \frac{R}{I} \right|^2 = \frac{R}{I} \cdot \frac{R^*}{I^*}$ and Power = $\frac{1}{2} \text{Re}(Z|v|^2)$
 Proof: Power = $\frac{1}{2} \text{Re}(Fv^*) = \frac{1}{2} \text{Re}(Zvv^*) = \frac{1}{2} \text{Re}(Z)|v|^2$ Now $v = -i\omega\phi$ so $|v|^2 = \omega^2|\phi|^2 = \omega^2|A|^2$

Standing waves - If some boundary condition $\Rightarrow \psi(\underline{r}, t) = 0$ for some $\underline{r} \Rightarrow$ standing wave solutions by virtue of no transmission past the boundary. (Effective $Z_2 = \infty$).
 i.e. for clamped string of length L, $\psi = 0$ at 0, L \Rightarrow condition of allowed ω 's of vibration. For standing wave solutions one may try SEPARABLE ψ 's and substitute into WAVE EQUATION and then solve subject to b.c.'s (i.e. $\psi(\underline{r}, t) = X(x)Y(y)Z(z)T(t)$) OR use 'no transmission' principle and superpose permutations of $\psi = A e^{i(k \cdot \underline{r} - \omega t)}$ or different k 's. Either way solution will be QUANTISED by b.c.'s - for a string clamped, $\psi(x, t) = 2A \sin kx \sin \omega t$, $kL = n\pi$ by b.c.s $\Rightarrow k = \frac{n\pi}{L}$ ($n \in \mathbb{Z}$)
 $\Rightarrow \omega = v n \frac{\pi}{L}$. For a 2D plate $\omega = v \pi \sqrt{\frac{n^2}{a^2} + \frac{m^2}{b^2}}$, for a 3D box $\omega = v \pi \sqrt{\frac{n^2}{a^2} + \frac{m^2}{b^2} + \frac{l^2}{c^2}}$
 with $m, n, l \in \mathbb{Z}$.

For longitudinal waves see 'Elastic waves' (Dynamics) section. Note ACOUSTIC IMPEDANCE for pressure waves in a gas = 'Excess pressure/velocity' = $\sqrt{\rho P} = \rho v = \rho \frac{P}{\rho}$
 [$v_{\text{gas}} = \sqrt{\frac{P}{\rho}}$] $P = \text{pressure}$, $\rho = \text{density}$, $\rho = \frac{P}{v}$

Doppler effect for sound waves consider source moving at speed u , observer at speed w with source emitting sound at frequency f . Consider stationary observer at points ① and ②.

 Now ① and ② both measure speed of sound (in their frame) at $v = f\lambda$. From $S_{t=0}$ ① is a distance $f\lambda$ away and ② a distance $ut + f\lambda$ away. However, ① and ② measure sound frequencies different, denote f_1 and f_2
 $f_1 = f$, $f_2 = \frac{v}{\lambda_2}$ Now since:
 $ut + f\lambda_2 t = f\lambda t + wt \Rightarrow v + w = u + f\lambda_2$
 $\Rightarrow \lambda_2 = \frac{v + w - u}{f}$ Hence $f_2 = \frac{v f}{v + w - u} \therefore \frac{f_2}{f_1} = \frac{v}{v + w - u}$ Now observer at ② should measure the same value since they are at the same position except ② will measure v as $v - w$ since it is moving at tw relative to ②. So $\frac{f_2}{f_1} = \frac{v - w}{v - u}$

Dispersive waves A disturbance or WAVE PACKET may be a Fourier synthesis of many different frequency harmonic waves. Packet moves at GROUP VELOCITY v_g but individual waves may move at a different, PHASE VELOCITY, v_p . Hence DISPERSION.

 Now in packet point of max amplitude corresponds to point of ϕ at time t where all Fourier components have SAME PHASE = $kx - \omega t + \phi$. i.e. PHASE is independent of ω . Hence $\frac{d}{d\omega}(kx - \omega t + \phi) = 0 \Rightarrow t - \left(\frac{dk}{d\omega} \right) x = 0$ so need relation $v_g = v_p - \lambda \frac{dv_p}{d\lambda}$
 [v_g is AVERAGE group frequency] so $\frac{dx}{dt} = \left(\frac{d\omega}{dk} \right)_{\omega_0} = v_g(\omega_0)$ Note since $v_p k = \omega \Rightarrow v_g = v_p - \lambda \frac{dv_p}{d\lambda}$