

Diffraction

$$\text{Wavenumber} \quad k = \frac{2\pi}{\lambda}$$

$$\omega = 2\pi f \quad \text{Frequency}$$

$$\text{Wave speed} \quad c = f\lambda \quad \omega = ck$$

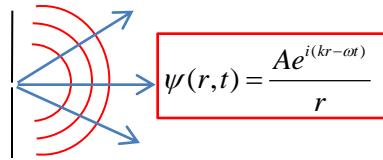
$$\text{Wave power input} \quad P = \frac{1}{2}ZA^2\omega^2$$

$$Z = \text{Wave impedance}$$

The Huygens-Fresnel Principle states: "Every unobstructed point of a wavefront, at a given instant, serves as a source of spherical secondary wavelets (with the same frequency as that of the primary wave). The amplitude of the optical field at any point beyond is the superposition of all these wavelets (considering their amplitudes and relative phases)."

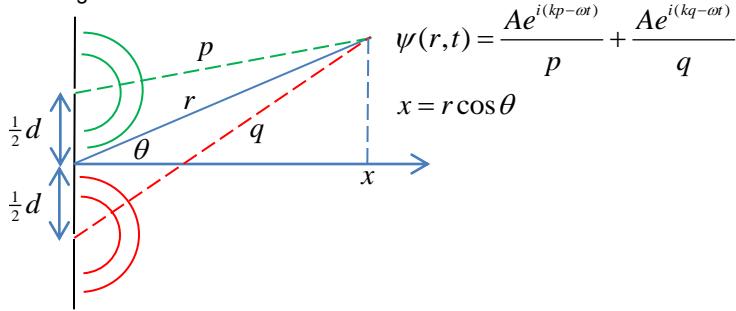
Hence to determine the *wavefield* beyond an illuminated edge of slit, we need to add up the effect of spherical wave sources in the vicinity of the slit or *aperture*.

An infinitesimally thin slit



Two infinitesimally thin slits

'Young's double slits'



Cosine Rule:

$$p^2 = r^2 + \frac{1}{4}d^2 - rd \cos(90^\circ - \theta)$$

$$p^2 = r^2 + \frac{1}{4}d^2 - rd \sin \theta$$

$$q^2 = r^2 + \frac{1}{4}d^2 - rd \cos(90^\circ + \theta)$$

$$p^2 = r^2 + \frac{1}{4}d^2 + rd \sin \theta$$

$$p = r \sqrt{1 + \frac{1}{4} \frac{d^2}{r^2} - \frac{d \sin \theta}{r}}$$

$$q = r \sqrt{1 + \frac{1}{4} \frac{d^2}{r^2} + \frac{d \sin \theta}{r}}$$

Assume $r \gg d$

$$\therefore \psi(r,t) \approx \frac{Ae^{-i\omega t}}{r} (e^{ikp} + e^{ikq})$$

Binomial expansion:

$$p \approx r + \frac{1}{8} \frac{d^2}{r} - \frac{1}{2} d \sin \theta$$

$$q \approx r + \frac{1}{8} \frac{d^2}{r} + \frac{1}{2} d \sin \theta$$

$$\therefore \psi(r,t) \approx \frac{Ae^{-i\omega t}}{r} e^{ik\left(r + \frac{1}{8} \frac{d^2}{r}\right)} (e^{-i\frac{1}{2}kd \sin \theta} + e^{i\frac{1}{2}kd \sin \theta})$$

$$\psi(r,t) \approx \frac{2Ae^{-i\omega t}}{r} e^{ik\left(r + \frac{1}{8} \frac{d^2}{r}\right)} \cos\left(\frac{1}{2}kd \sin \theta\right)$$

$$|\psi|^2 \approx \frac{A^2}{r^2} \cos^2\left(\frac{1}{2}kd \sin \theta\right) \quad \text{wave power}$$

Hence maxima when

$$\frac{1}{2}kd \sin \theta = n\pi \quad n \text{ is an integer}$$

$$\theta = \sin^{-1}\left(\frac{2n\pi}{kd}\right) = \sin^{-1}\left(\frac{n\lambda}{d}\right)$$

$$|n| < \frac{d}{\lambda}$$

$$\sin \theta = \cos(90^\circ - \theta)$$

$$-\sin \theta = \cos(90^\circ + \theta)$$

$$\cos x = \frac{1}{2}(e^{ix} + e^{-ix})$$

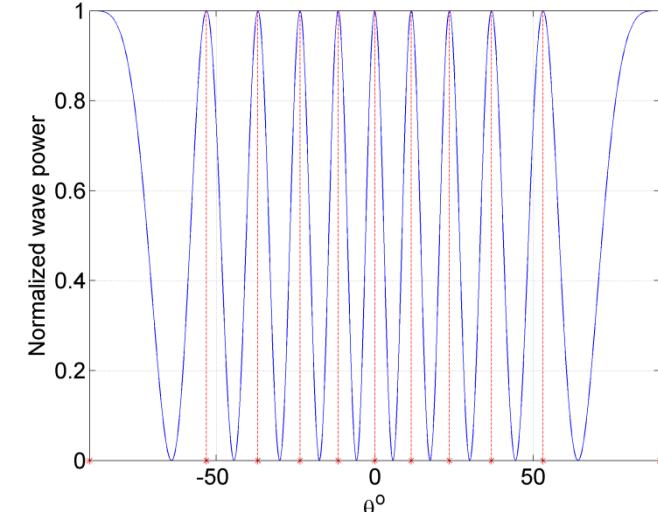
Equivalent geometry is
wavelet sources are at the
same angle (i.e. plane
waves) but separated by
 $d \sin \theta$

$$\text{Phase difference} \quad \Delta\phi = -\frac{1}{2}kd \sin \theta$$



$$\text{Phase difference} \quad \Delta\phi = \frac{1}{2}kd \sin \theta$$

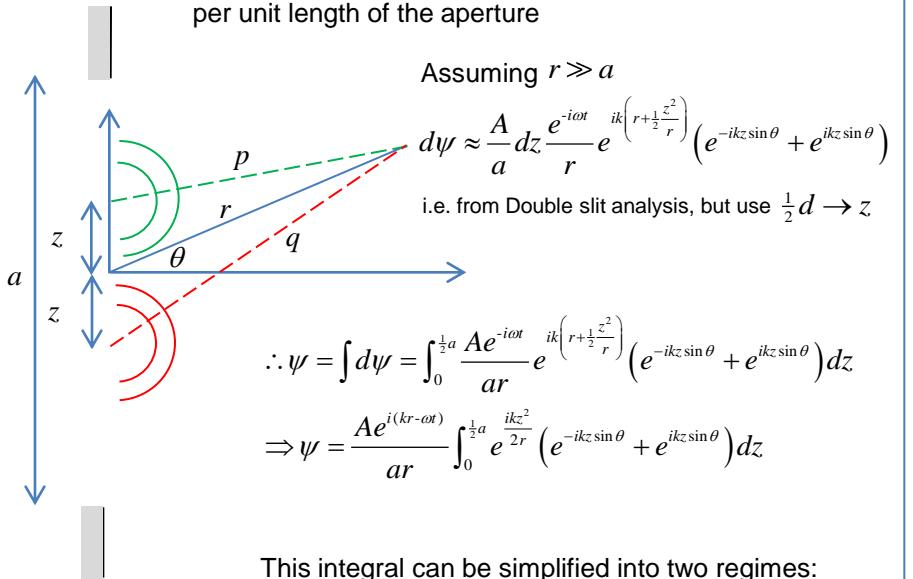
Youngs Double slits: $\lambda = 650\text{nm}$, $d = 5\lambda$



The diffraction pattern of a finite width slit

The analysis of the double slit can be extended to include pairs of infinitesimal slits which cover the whole aperture width a

Define A/a in this case to be the illumination amplitude per unit length of the aperture



Fraunhofer – or ‘linear phase’ with z $e^{\frac{ikz^2}{2r}} \approx \text{constant}$

$$\frac{k\left(\frac{1}{2}a\right)^2}{2r} \ll 1$$

$$\frac{2\pi a^2}{8\lambda r} \ll 1$$

$$r \gg \frac{\pi a^2}{4\lambda}$$

$$r \gg \frac{a^2}{\lambda}$$

$$\psi = \frac{Ae^{i(kr-\omega t)}}{ar} \int_0^{\frac{1}{2}a} (e^{-ikz \sin \theta} + e^{ikz \sin \theta}) dz$$

$$\psi = \frac{2Ae^{i(kr-\omega t)}}{ar} \int_0^{\frac{1}{2}a} \cos(kz \sin \theta) dz$$

$$\psi = \frac{2Ae^{i(kr-\omega t)}}{ar} \left[\frac{\sin(kz \sin \theta)}{k \sin \theta} \right]_0^{\frac{1}{2}a}$$

$$|\psi|^2 = \frac{A^2}{r^2} \left(\frac{\sin\left(\frac{1}{2}ka \sin \theta\right)}{\frac{1}{2}ka \sin \theta} \right)^2$$

$$\theta = 0; \quad |\psi|^2 = |\psi_0|^2 = \frac{A^2}{r^2}$$

$$\therefore \left| \frac{\psi}{\psi_0} \right|^2 = \left(\frac{\sin\left(\frac{1}{2}ka \sin \theta\right)}{\frac{1}{2}ka \sin \theta} \right)^2$$

Hence zeros when:

$$\frac{1}{2}kd \sin \theta = n\pi \quad n \text{ is a non-zero integer}$$

$$\theta = \sin^{-1}\left(\frac{2n\pi}{kd}\right) \quad |n| < \frac{kd}{2\pi}$$

Fresnel – or ‘quadratic phase’ with z

$$\theta = 0^\circ$$

$$\psi = \frac{Ae^{i(kr-\omega t)}}{ar} \int_0^{\frac{1}{2}a} e^{\frac{ikz^2}{2r}} dz$$

$$\psi = \frac{Ae^{i(kr-\omega t)}}{ar} \int_0^{\frac{1}{2}a} e^{\frac{i\pi z^2}{\lambda r}} dz$$

$$\frac{1}{2}\pi t^2 = \frac{\pi z^2}{\lambda r} \Rightarrow t = z\sqrt{\frac{2}{\lambda r}} \quad k = \frac{2\pi}{\lambda}$$

$$\psi = \frac{Ae^{i(kr-\omega t)}}{ar} \sqrt{\frac{1}{2}\lambda r} \int_0^{\frac{1}{2}a} \sqrt{\frac{2}{\lambda r}} (\cos(\frac{1}{2}\pi t^2) + i \sin(\frac{1}{2}\pi t^2)) dt$$

$$|\psi|^2 = \frac{A^2 \lambda}{2a^2 r} |C(w) + iS(w)|^2$$

$$w = \frac{1}{2}a\sqrt{\frac{2}{\lambda r}}$$

$$C(w) = \int_0^w \cos\left(\frac{1}{2}\pi t^2\right) dt$$

$$S(w) = \int_0^w \sin\left(\frac{1}{2}\pi t^2\right) dt$$

$$w^2 = \frac{1}{4}a^2 \frac{2}{\lambda r}$$

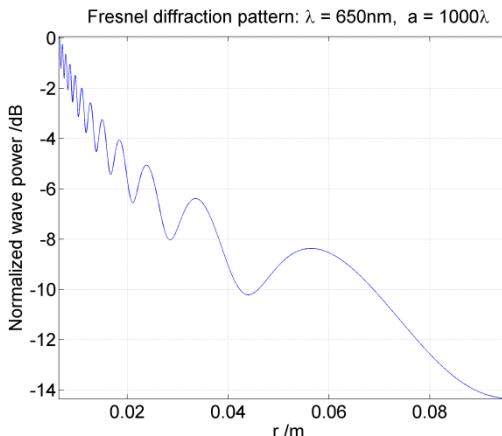
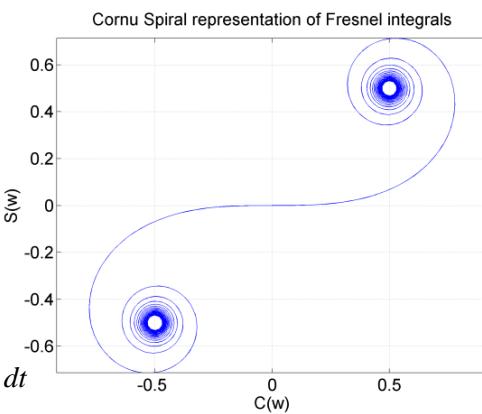
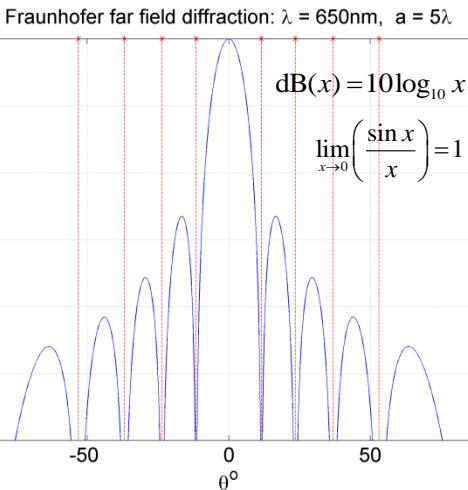
$$r = \frac{a^2}{2\lambda w^2}$$

$$r \gg a$$

$$\therefore \frac{a^2}{2\lambda w^2} \gg a$$

$$\lambda \ll \frac{a}{2w^2}$$

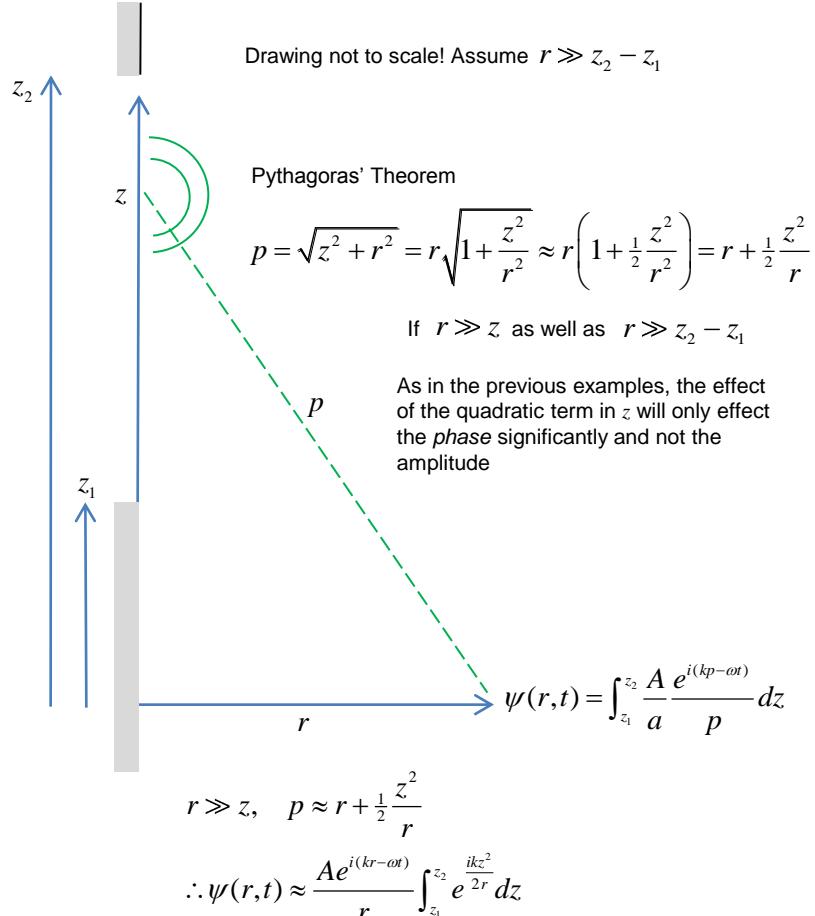
Fresnel Integrals
These can't be evaluated exactly, but can be evaluated numerically



Generalized Fresnel wavefield

We can derive the Fresnel regime wavefield for more general geometries, and apply this to determine the diffraction pattern of a 'knife edge.'

Consider the uniformly illuminated aperture to extend from z_1 to z_2 .



In this case, absorb a into constant A which could be calculated by direct wave intensity measurement.

$$k = \frac{2\pi}{\lambda}$$

$$\psi = \frac{A e^{i(kr - \omega t)}}{r} \int_{z_1}^{z_2} e^{\frac{i\pi z^2}{\lambda r}} dz$$

$$\psi = \frac{A e^{i(kr - \omega t)}}{r} \sqrt{\frac{1}{2}\lambda r} \int_{z_1}^{z_2} \frac{\sqrt{\frac{2}{\lambda r}}}{\sqrt{\frac{1}{2}\lambda r}} (\cos(\frac{1}{2}\pi t^2) + i \sin(\frac{1}{2}\pi t^2)) dt$$

$$|\psi|^2 = \frac{A^2 \lambda}{2r} |C(w_2) - C(w_1) + iS(w_2) - iS(w_1)|^2$$

$$w_{1,2} = z_{1,2} \sqrt{\frac{2}{\lambda r}}$$

$$C(w) = \int_0^w \cos(\frac{1}{2}\pi t^2) dt$$

$$S(w) = \int_0^w \sin(\frac{1}{2}\pi t^2) dt$$

Now for a 'knife edge'

$$z_1 = z, \quad z_2 = \infty$$

$$|\psi|^2 = \frac{A^2 \lambda}{2r} |C(\infty) - C(w) + iS(\infty) - iS(w)|^2$$

$$w = z \sqrt{\frac{2}{\lambda r}}$$

From the Cornu Spiral one can see that

$$S(\infty) = C(\infty) = \frac{1}{2}$$

$$\therefore |\psi|^2 = \frac{A^2 \lambda}{2r} \left| \frac{1}{2}(1+i) - C(w) - iS(w) \right|^2$$

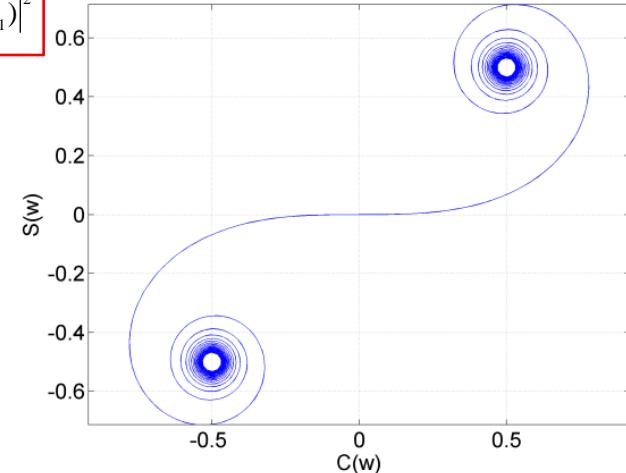
Now if we are *above* the knife edge by z (rather than below) we must exchange its sign. Since w is proportional to z :

$$|\psi|^2 = \frac{A^2 \lambda}{2r} \left| \frac{1}{2}(1+i) + C(w) + iS(w) \right|^2$$

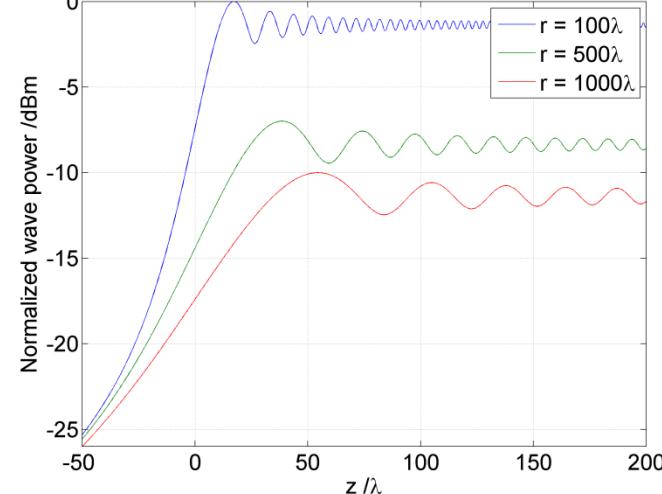
$$w = z \sqrt{\frac{2}{\lambda r}}$$

$$\text{Consider substitution } \frac{1}{2}\pi t^2 = \frac{\pi z^2}{\lambda r} \Rightarrow t = z \sqrt{\frac{2}{\lambda r}} \Rightarrow dz = dt \sqrt{\frac{2}{\lambda r}}$$

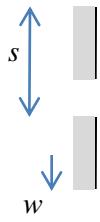
Cornu Spiral representation of Fresnel integrals



Fresnel knife edge diffraction pattern: $\lambda = 650\text{nm}$



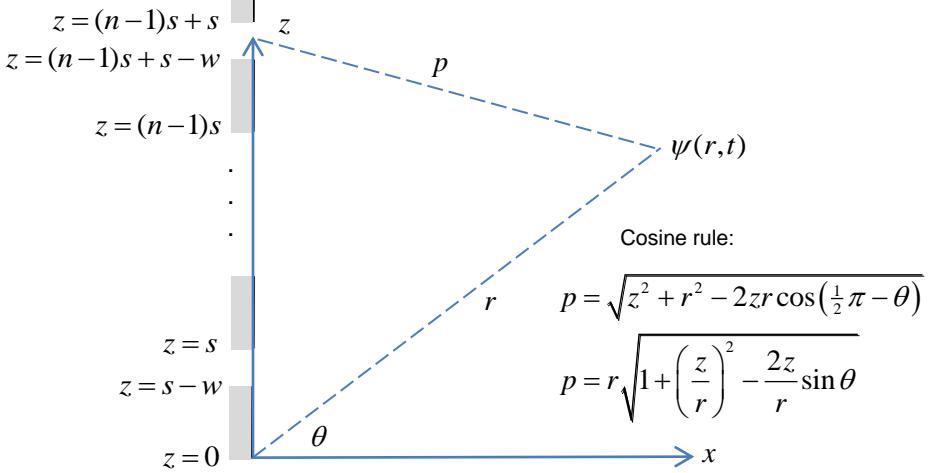
Far-field (Fraunhofer) diffraction pattern of a grating



Assume the grating is uniformly illuminated, and consists of N slits of width w , separated by spacing s .

$$\psi(r, t) = \sum_{n=1}^N \int_{s-w+(n-1)s}^{s+(n-1)s} \frac{Adz}{Nw} \times \frac{e^{i(kp-\omega t)}}{p}$$

$$\psi(r, t) = \frac{Ae^{-i\omega t}}{Nw} \sum_{n=1}^N \int_{ns-w}^{ns} \frac{e^{ikp}}{p} dz$$



Assume 'far-field' (Fraunhofer) scenario – i.e. $r \gg z$

$$\therefore p \approx r \left(1 - \frac{z}{r} \sin \theta\right) = r - z \sin \theta \quad \text{i.e. plane waves arriving at } r, \theta$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nwr} \sum_{n=1}^N \int_{ns-w}^{ns} e^{-ikz \sin \theta} dz$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nwr} \sum_{n=1}^N \left[\frac{e^{-ikz \sin \theta}}{-ik \sin \theta} \right]_{ns-w}^{ns}$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nwr} \sum_{n=1}^N \frac{1}{-ik \sin \theta} \left(e^{-ikns \sin \theta} - e^{-ik(ns-w) \sin \theta} \right)$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nwr} \sum_{n=1}^N \frac{1}{-ik \sin \theta} e^{-ik(ns-\frac{1}{2}w) \sin \theta} \left(e^{-ik\frac{1}{2}ws \sin \theta} - e^{ik\frac{1}{2}ws \sin \theta} \right)$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nr} \frac{1}{\frac{1}{2}kw \sin \theta} \frac{1}{2i} \left(e^{ik\frac{1}{2}ws \sin \theta} - e^{-ik\frac{1}{2}ws \sin \theta} \right) \sum_{n=1}^N e^{-ik(ns-\frac{1}{2}w) \sin \theta}$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nr} \frac{\sin(\frac{1}{2}kw \sin \theta)}{\frac{1}{2}kw \sin \theta} e^{-ik\frac{1}{2}ws \sin \theta} \sum_{n=1}^N \left(e^{-iks \sin \theta} \right)^n$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nr} \frac{\sin(\frac{1}{2}kw \sin \theta)}{\frac{1}{2}kw \sin \theta} e^{-ik\frac{1}{2}ws \sin \theta} \frac{e^{-iks \sin \theta} - e^{-ik(N+1)s \sin \theta}}{1 - e^{-iks \sin \theta}}$$

The last step uses the formula for the sum of a *geometric series*

$$\sum_{n=1}^N ar^{n-1} = a + ar + \dots + ar^{N-1} = a \frac{1-r^N}{1-r} \quad \therefore a \frac{1-r^N}{1-r} = \frac{a}{r} \sum_{n=1}^N r^n \Rightarrow \sum_{n=1}^N r^n = \frac{r-r^{N+1}}{1-r}$$

$$\therefore \psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nr} \frac{\sin(\frac{1}{2}kw \sin \theta)}{\frac{1}{2}kw \sin \theta} e^{-ik\frac{1}{2}ws \sin \theta} \frac{e^{-iks \sin \theta} e^{-i\frac{1}{2}kNs \sin \theta} \left(e^{i\frac{1}{2}kNs \sin \theta} - e^{-i\frac{1}{2}kNs \sin \theta} \right)}{e^{-i\frac{1}{2}ks \sin \theta} \left(e^{i\frac{1}{2}ks \sin \theta} - e^{-i\frac{1}{2}ks \sin \theta} \right)}$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nr} \frac{\sin(\frac{1}{2}kw \sin \theta)}{\frac{1}{2}kw \sin \theta} e^{-ik\frac{1}{2}ws \sin \theta} \frac{e^{-i\frac{1}{2}ks \sin \theta} e^{-i\frac{1}{2}kNs \sin \theta} \times 2i \sin(\frac{1}{2}kNs \sin \theta)}{2i \sin(\frac{1}{2}ks \sin \theta)}$$

$$\psi(r, t) \approx \frac{Ae^{i(kr-\omega t)}}{Nr} \frac{\sin(\frac{1}{2}kw \sin \theta)}{\frac{1}{2}kw \sin \theta} e^{-ik\frac{1}{2}(w+s+Ns) \sin \theta} \frac{\sin(\frac{1}{2}kNs \sin \theta)}{\sin(\frac{1}{2}ks \sin \theta)}$$

$$|\psi|^2 \approx \frac{A^2}{N^2 r^2} \left(\frac{\sin(\frac{1}{2}kw \sin \theta)}{\frac{1}{2}kw \sin \theta} \times \frac{\sin(\frac{1}{2}kNs \sin \theta)}{\sin(\frac{1}{2}ks \sin \theta)} \right)^2$$

$$|\psi|^2 \approx \frac{A^2}{N^2 r^2} \left(\frac{\sin(\frac{\pi}{\lambda} ws \sin \theta)}{\frac{\pi}{\lambda} ws \sin \theta} \times \frac{\sin(\frac{\pi}{\lambda} Ns \sin \theta)}{\sin(\frac{\pi}{\lambda} s \sin \theta)} \right)^2$$

$$\leftarrow k = \frac{2\pi}{\lambda} \text{ wavenumber}$$

Zeros at: $\frac{\pi}{\lambda} ws \sin \theta = n\pi$

$$\theta = \sin^{-1} \left(\frac{n\lambda}{w} \right)$$

$$n \in \mathbb{Z}, n \neq 0$$

Maxima ('grating lobes') at: $\frac{\pi}{\lambda} Ns \sin \theta = m\pi$

$$\theta = \sin^{-1} \left(\frac{m\lambda}{Ns} \right)$$

$$m \in \mathbb{Z}$$

Maxima ('grating lobes') at: $\frac{\pi}{\lambda} s \sin \theta = q\pi$

$$\theta = \sin^{-1} \left(\frac{q\lambda}{s} \right)$$

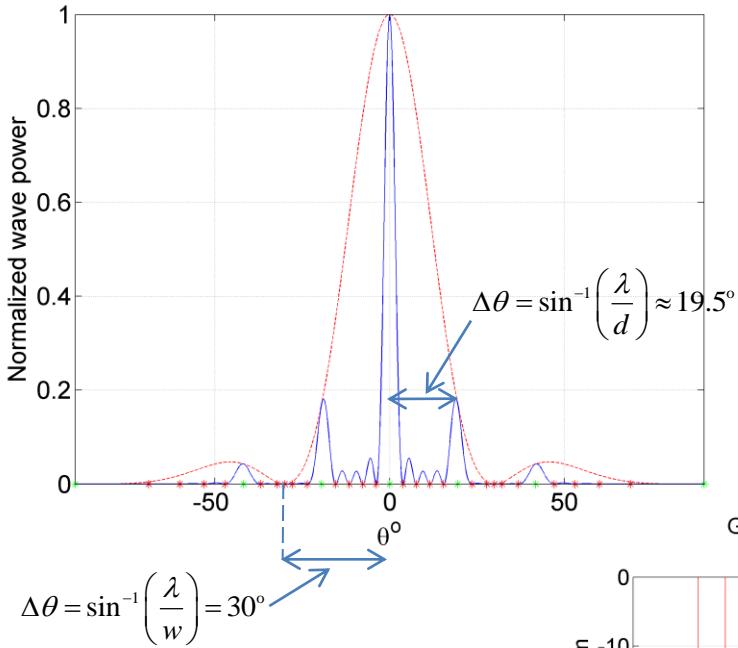
$$q \in \mathbb{Z}$$

Far-Field diffraction summary

This is the actual formula for the **diffraction pattern wave power**. It incorporates all the maxima and minima effects described above.

$$|\psi|^2 = \frac{A^2}{N^2 r^2} \left(\frac{\sin(\frac{\pi}{\lambda} w \sin \theta)}{\frac{\pi}{\lambda} w \sin \theta} \times \frac{\sin(\frac{\pi}{\lambda} N s \sin \theta)}{\sin(\frac{\pi}{\lambda} s \sin \theta)} \right)^2$$

Grating Fraunhofer far field diffraction
 $\lambda = 650\text{nm}$, $s = 3\lambda$, $w = 2\lambda$, $N = 5$



Almost all of these diffraction effects result in a **main lobe** of angular width (in radians)

$$\Delta\theta \approx \frac{\lambda}{d}$$

where d is a characteristic length of the grating, slit etc. For any optical instrument, the 'resolving power' is likely to be diffraction limited. So this ratio gives the **minimum angular deviation** that two objects could be **resolved** via an optical system.

e.g. for the James Web space telescope, $d = 6.5\text{m}$. So for Infra-Red light of wavelength $3.15\mu\text{m}$, $\Delta\theta$ is about 0.1 arc-seconds*.

n, m, p are integers

Envelope due to finite slit width

$$\text{Zeros at: } \theta = \sin^{-1}\left(\frac{n\lambda}{w}\right); n \neq 0$$

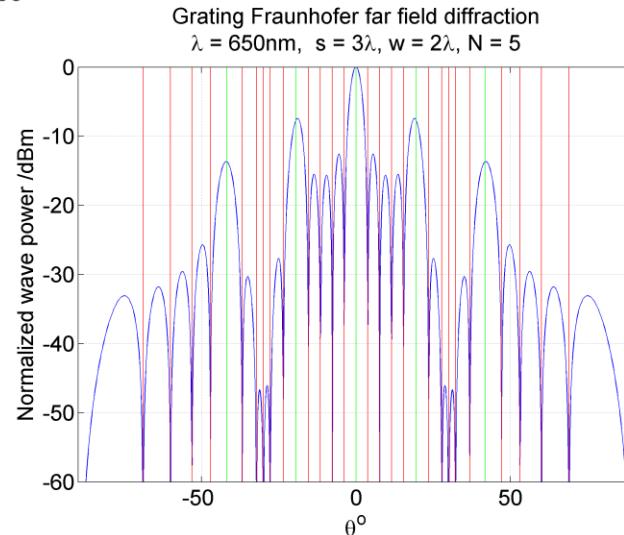
Maxima due to slit spacing

$$\text{Maxima at: } \theta = \sin^{-1}\left(\frac{m\lambda}{s}\right)$$

Fine structure due to number of slits
 (i.e. overall size of aperture)

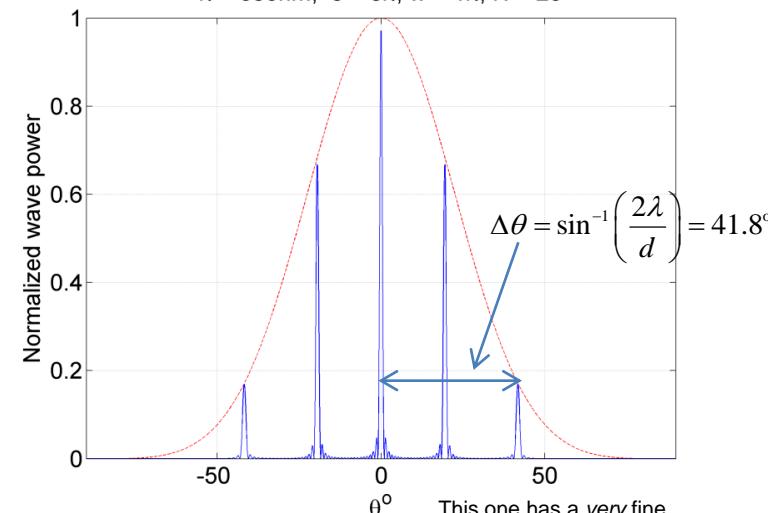
$$\text{Zeros at: } \theta = \sin^{-1}\left(\frac{p\lambda}{Ns}\right)$$

But maxima when $\frac{p}{N}$ integer m



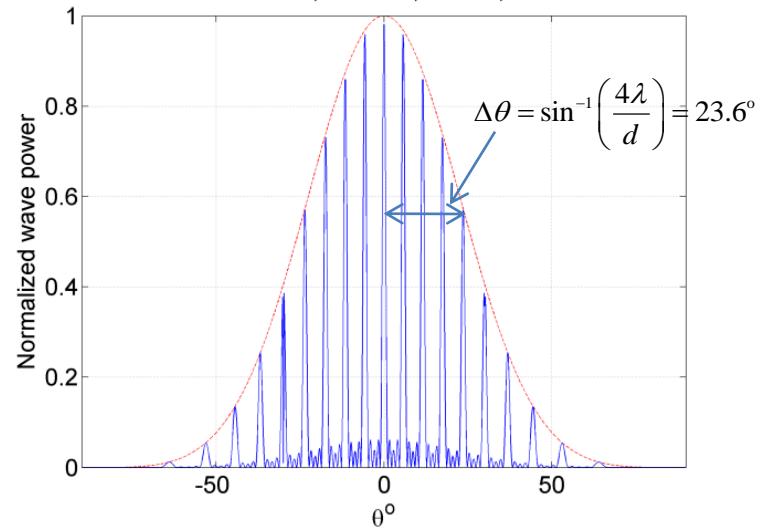
Grating Fraunhofer far field diffraction

$\lambda = 650\text{nm}$, $s = 3\lambda$, $w = 1\lambda$, $N = 20$



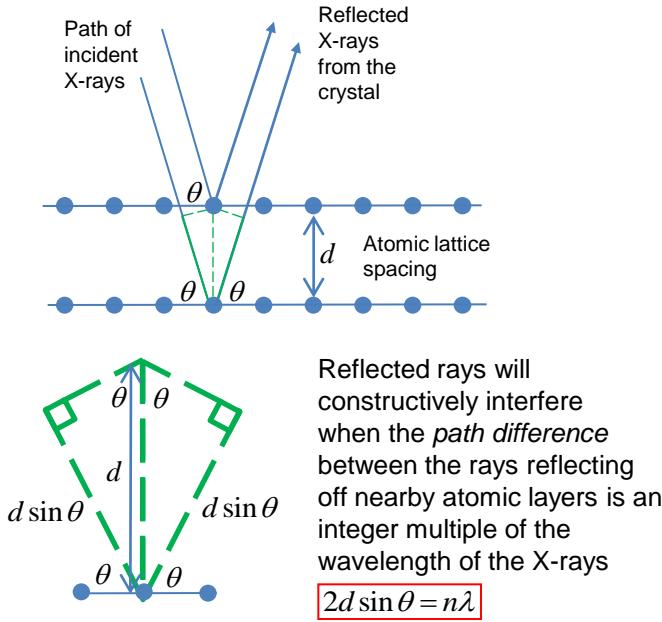
Grating Fraunhofer far field diffraction

$\lambda = 650\text{nm}$, $s = 10\lambda$, $w = 1\lambda$, $N = 5$

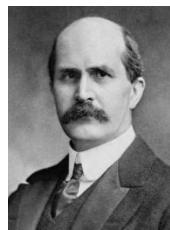


*1 arc-second is $1/3600$ of a degree

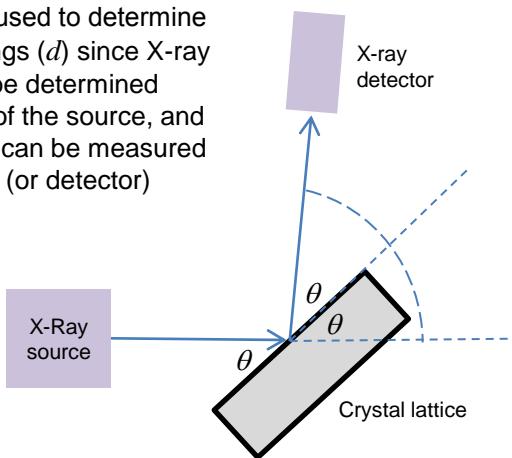
Bragg's law of X-ray diffraction from atoms in a crystal lattice



Bragg's law can be used to determine atomic lattice spacings (d) since X-ray wavelengths λ can be determined from the properties of the source, and the diffraction angle can be measured via rotating a crystal (or detector) as shown



Sir William Henry Bragg 1862-1942



Modelling general diffraction effects from a finite width slit

We can use a computer to evaluate the wavefield in the vicinity of a finite width slit which is uniformly illuminated. We are therefore not restricted to the limitations of the Fraunhofer and Fresnel regimes

