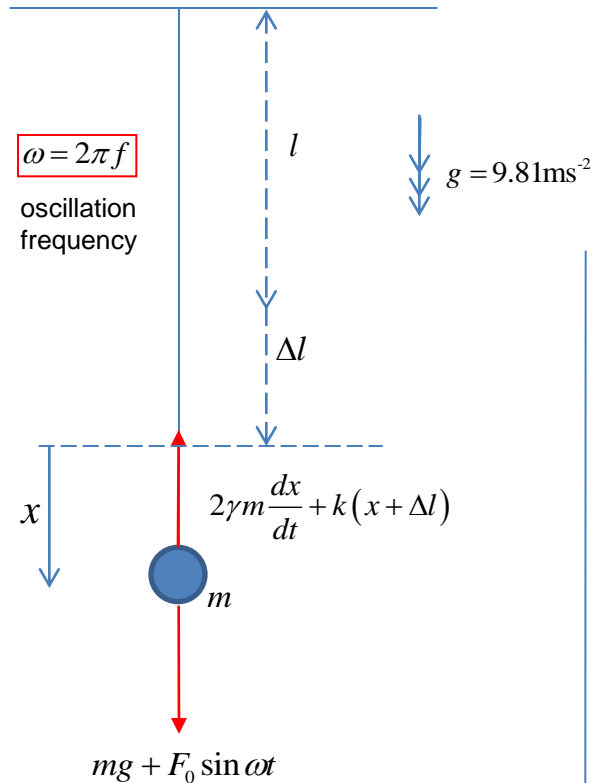


## SHM equation from driven mechanical oscillations



By Newton's Second Law:

$$m \frac{d^2 x}{dt^2} = mg + F_0 \sin \omega t - 2\gamma m \frac{dx}{dt} - k(x + \Delta l)$$

At equilibrium  $x = 0$ ,  $F_0 = 0$

$$0 = mg - k\Delta l \quad \therefore \Delta l = \frac{mg}{k}$$

$$\text{Hence: } m \frac{d^2 x}{dt^2} + 2\gamma m \frac{dx}{dt} + kx = F_0 \sin \omega t$$

Consider a particle of mass  $m$  suspended from a light elastic string from a fixed surface. The string has natural length  $l$ . Assume a *Hookean* law of elasticity i.e. restoring force is proportional to extension. The elastic constant in this case is  $k$ . Also assume mass is subject to air resistance which is proportional to velocity and mass  $m$ . The mass is also pulled 'driven' via an oscillatory force of magnitude  $F_0$  and frequency  $f = \omega/2\pi$ .

In the absence of any driving force, the mass rests at string extension  $\Delta l$ . It is assumed at time  $t = 0$  that extension from this equilibrium point,  $(x)$ , is zero and the mass is at instantaneous rest.

$$\frac{d^2 x}{dt^2} + 2\gamma \frac{dx}{dt} + \frac{k}{m} x = \frac{F_0}{m} \sin \omega t$$

This equation has a very similar form to the generic equation of **Simple Harmonic Motion (SHM)**

$$\frac{d^2 x}{dt^2} + 2\gamma \frac{dx}{dt} + \omega_0^2 x = A_0 \omega_0^2 \sin \omega t$$

$$\omega_0 = \frac{k}{m}, \quad A_0 \omega_0^2 = \frac{F_0}{m}$$

The **general solution** to this *inhomogeneous, second order differential equation* has the form  $x(t) = X(t) + Y(t)$

$$\text{where } \frac{d^2 X}{dt^2} + 2\gamma \frac{dX}{dt} + \omega_0^2 X = 0$$

$$\text{and } Y(t) = A \sin(\omega t - \phi)$$

i.e. a similar form (and frequency) to the driving force term. Experiments indicate that the latter, when damping is "low", corresponds to the steady state condition of the system. i.e. the  $X(t)$  term decays with time and therefore is *transient*.\*

It will be shown (on the next few pages) that oscillatory solutions are possible when the system is *under-damped*. This is when

$$\omega_0 > \gamma$$

Lets consider the steady state solutions, and substitute into the SHM equation

$$x = A \sin(\omega t - \phi)$$

$$-\omega^2 A \sin(\omega t - \phi) + 2\gamma \omega A \cos(\omega t - \phi) + \omega_0^2 A \sin(\omega t - \phi) = A_0 \omega_0^2 \sin \omega t$$

$$(\omega_0^2 - \omega^2) A \sin(\omega t - \phi) + 2\gamma \omega A \cos(\omega t - \phi) = A_0 \omega_0^2 \sin \omega t$$

$$\therefore (\omega_0^2 - \omega^2) (\sin \omega t \cos \phi - \cos \omega t \sin \phi) + \dots$$

$$2\gamma \omega (\cos \omega t \cos \phi + \sin \omega t \sin \phi) = \frac{A_0 \omega_0^2}{A} \sin \omega t$$

$$((\omega_0^2 - \omega^2) \cos \phi + 2\gamma \omega \sin \phi) \sin \omega t + \dots$$

$$-(\omega_0^2 - \omega^2) \sin \phi + 2\gamma \omega \cos \phi) \cos \omega t = \frac{A_0 \omega_0^2}{A} \sin \omega t$$

Comparing coefficients of  $\sin \omega t$  and  $\cos \omega t$

$$(\omega_0^2 - \omega^2) \cos \phi + 2\gamma \omega \sin \phi = \frac{A_0 \omega_0^2}{A}$$

$$-(\omega_0^2 - \omega^2) \sin \phi + 2\gamma \omega \cos \phi = 0$$

See next page for algebra

$$\therefore \tan \phi = \frac{2\gamma \omega}{\omega_0^2 - \omega^2}$$

and

$$A = \frac{A_0 \omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2 \omega^2}}$$

$$(\omega_0^2 - \omega^2) \cos \phi + 2\gamma\omega \sin \phi = \frac{A_0\omega_0^2}{A}$$

$$(\omega_0^2 - \omega^2) + 2\gamma\omega \tan \phi = \frac{A_0\omega_0^2}{A \cos \phi}$$

$$(\omega_0^2 - \omega^2) + 2\gamma\omega \tan \phi = \frac{A_0\omega_0^2}{A} \sqrt{1 + \tan^2 \phi}$$

$$\tan \phi = \frac{2\gamma\omega}{\omega_0^2 - \omega^2}$$

$$(\omega_0^2 - \omega^2) + 2\gamma\omega \frac{2\gamma\omega}{\omega_0^2 - \omega^2} = \frac{A_0\omega_0^2}{A} \sqrt{1 + \frac{4\gamma^2\omega^2}{(\omega_0^2 - \omega^2)^2}}$$

$$\frac{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}{\omega_0^2 - \omega^2} = \frac{A_0\omega_0^2}{A} \frac{1}{\omega_0^2 - \omega^2} \sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}$$

$$A = \frac{A_0\omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}}$$

Now A has a maxima when

$$\frac{dA}{d\omega} = 0$$

$$\frac{dA}{d\omega} = -\frac{1}{2} \frac{A_0\omega_0^2 (2(\omega_0^2 - \omega^2)(-2\omega) + 8\gamma^2\omega)}{\left((\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2\right)^{\frac{3}{2}}}$$

$$\frac{dA}{d\omega} = \frac{2A_0\omega_0^2\omega(\omega_0^2 - \omega^2 - 2\gamma^2)}{\left((\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2\right)^{\frac{3}{2}}}$$

$$\frac{dA}{d\omega} = 0 \Rightarrow \omega_0^2 - \omega^2 - 2\gamma^2 = 0$$

$$\therefore \omega_{\max} = \sqrt{\omega_0^2 - 2\gamma^2}$$

$$\omega = \sqrt{\omega_0^2 - 2\gamma^2}$$

$$\therefore (\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2$$

$$= (\omega_0^2 - \omega_0^2 - 2\gamma^2)^2 + 4\gamma^2(\omega_0^2 - 2\gamma^2)$$

$$= 4\gamma^4 + 4\gamma^2\omega_0^2 - 8\gamma^4$$

$$= 4\gamma^2\omega_0^2 - 4\gamma^4$$

$$\therefore A_{\max} = \frac{A_0\omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}}$$

$$A_{\max} = \frac{A_0\omega_0^2}{\sqrt{4\gamma^2\omega_0^2 - 4\gamma^4}}$$

$$A_{\max} = \frac{A_0\omega_0^2}{2\gamma\sqrt{\omega_0^2 - \gamma^2}}$$

$$x = A \sin(\omega t - \phi) \rightarrow$$

### Steady-State SHM Summary

$$\frac{d^2x}{dt^2} + 2\gamma \frac{dx}{dt} + \omega_0^2 x = A_0\omega_0^2 \sin \omega t$$

$$x = \frac{A_0\omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2\omega^2}} \sin(\omega t - \phi)$$

$$\phi = \tan^{-1} \left( \frac{2\gamma\omega}{\omega_0^2 - \omega^2} \right)$$

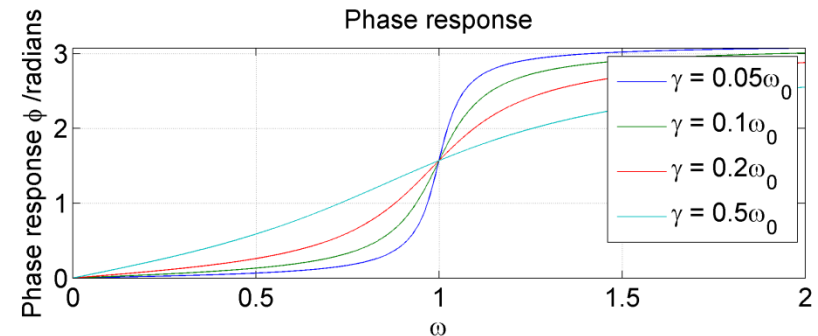
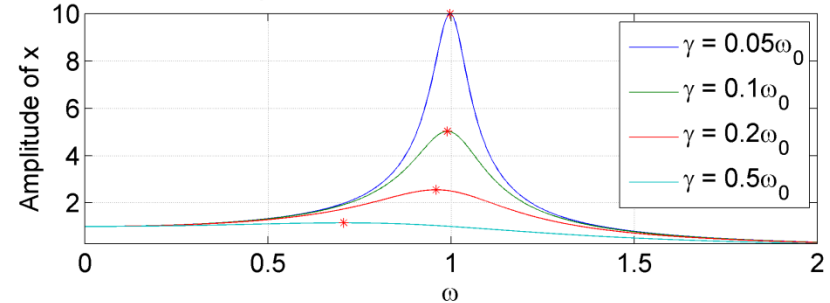
$$|x|_{\max} \text{ when } \omega = \sqrt{\omega_0^2 - 2\gamma^2}$$

$$|x|_{\max} = \frac{A_0\omega_0^2}{2\gamma\sqrt{\omega_0^2 - \gamma^2}}$$

As the damping factor approaches the 'natural frequency'  $\omega_0$ , the height of the **resonance** peak increases and the peak sharpens.

When the driving frequency approaches the natural frequency the phase of the steady state response approaches  $90^\circ$ . As the driving frequency increases, the steady state response will tend towards  $180^\circ$  out of phase with the driving oscillator.

Steady state solution to driven SHM equation



Solving the **SHM equation** (steady state) using **complex variables**. i.e. we make use of **De-Moivre's Theorem**

$$\frac{d^2 z}{dt^2} + 2\gamma \frac{dz}{dt} + \omega_0^2 z = A_0 \omega_0^2 e^{i\omega t}$$

$$z = Ae^{i(\omega t - \phi)}$$

$$(-\omega^2 + 2i\gamma\omega + \omega_0^2) Ae^{i(\omega t - \phi)} = A_0 \omega_0^2 e^{i\omega t}$$

$$(-\omega^2 + 2i\gamma\omega + \omega_0^2) Ae^{-i\phi} = A_0 \omega_0^2$$

i.e. the steady state solution  $x = A \sin(\omega t - \phi)$  is the *imaginary* part of  $z$

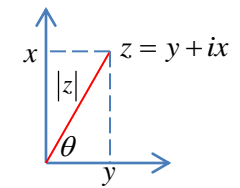
$$\text{Im}(A_0 e^{i\omega t}) = \text{Im}(A_0 \cos \omega t + i \sin \omega t) = A_0 \sin \omega t$$

$$\text{Im}(Ae^{i(\omega t - \phi)}) = \text{Im}(A \cos \omega t + i A \sin \omega t) = A \sin(\omega t - \phi)$$

$$z = y + ix$$

$$|z| = \sqrt{x^2 + y^2}$$

$$\arg z = \tan^{-1} \frac{x}{y}$$



$$e^{i\theta} = \cos \theta + i \sin \theta$$

$$z = |z| e^{i\theta}$$

$$\arg z = \theta$$

Yes I know  $x, y$  appear to be the wrong way round, but the use of  $\sin$  in our forcing frequency means  $x$  associates with the imaginary part. It is merely for convenience!

Compute the modulus (complex number magnitude)

$$|-\omega^2 + 2i\gamma\omega + \omega_0^2| A = A_0 \omega_0^2 |e^{i\phi}| = A_0 \omega_0^2$$

$$A = \frac{A_0 \omega_0^2}{|-\omega^2 + 2i\gamma\omega + \omega_0^2|}$$

$$\therefore A = \frac{A_0 \omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2 \omega^2}}$$

Compute the modulus (complex number magnitude)

$$(-\omega^2 + 2i\gamma\omega + \omega_0^2) A = A_0 \omega_0^2 e^{i\phi}$$

$$A |-\omega^2 + 2i\gamma\omega + \omega_0^2| e^{i \arg(-\omega^2 + 2i\gamma\omega + \omega_0^2)} = A_0 \omega_0^2 e^{i\phi}$$

$$|-\omega^2 + 2i\gamma\omega + \omega_0^2| A = A_0 \omega_0^2$$

$$\therefore \phi = \arg(-\omega^2 + 2i\gamma\omega + \omega_0^2)$$

$$\therefore \phi = \tan^{-1} \left( \frac{2\gamma\omega}{\omega_0^2 - \omega^2} \right)$$

### Steady-State SHM Summary

$$\frac{d^2 x}{dt^2} + 2\gamma \frac{dx}{dt} + \omega_0^2 x = A_0 \omega_0^2 \sin \omega t$$

$$x = \frac{A_0 \omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2 \omega^2}} \sin(\omega t - \phi)$$

$$\phi = \tan^{-1} \left( \frac{2\gamma\omega}{\omega_0^2 - \omega^2} \right)$$

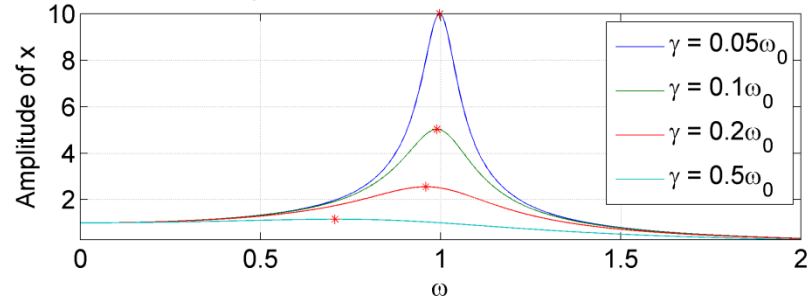
$$|x|_{\max} \text{ when } \omega = \sqrt{\omega_0^2 - 2\gamma^2}$$

$$|x|_{\max} = \frac{A_0 \omega_0^2}{2\gamma \sqrt{\omega_0^2 - \gamma^2}}$$

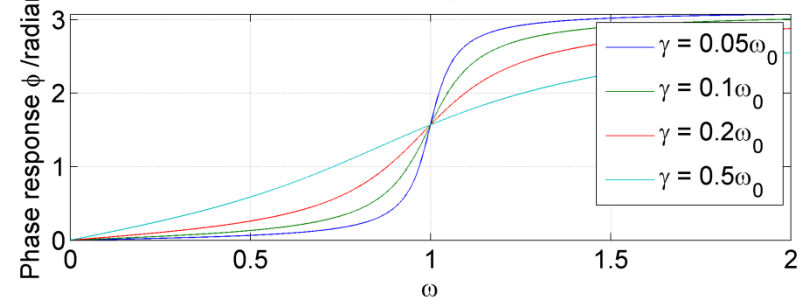
As you can see, this is a far more efficient method of arriving at the steady state solution.

We will therefore adopt a complex number from now on.

Steady state solution to driven SHM equation



Phase response



## General solution of the Forced SHM equation i.e. including the *transient* term

### The equation of forced SHM

$$\frac{d^2x}{dt^2} + 2\gamma \frac{dx}{dt} + \omega_0^2 x = A_0 \omega_0^2 \sin \omega t$$

### General solution

We shall exploit the *linearity* of the SHM equation by expressing the general solution  $x(t)$  in terms of a *Complementary Function*  $X$  (which is the solution when  $A_0 = 0$ ) plus a *Particular Integral*  $B$ , which will have the same functional form as the 'forcing term'.

$$x = X + Y$$

$$X = Ae^{qt} \quad \text{i.e. guess solutions of this form}$$

$$Y = B \sin(\omega t - \phi)$$

$$\frac{d^2X}{dt^2} + 2\gamma \frac{dX}{dt} + \omega_0^2 X = 0$$

$$q^2 Ae^{qt} + 2\gamma q Ae^{qt} + \omega_0^2 Ae^{qt} = 0$$

$$q^2 + 2\gamma q + \omega_0^2 = 0$$

$$q = \frac{-2\gamma \pm \sqrt{4\gamma^2 - 4\omega_0^2}}{2}$$

$$q = -\gamma \pm \sqrt{\gamma^2 - \omega_0^2}$$

$$q = -\gamma \pm i\sqrt{\omega_0^2 - \gamma^2} \quad \text{alternative!}$$

$X(t)$  must be a superposition of *two* solutions in general, since the SHM equation is second order. i.e. two integrations to solve and therefore two integration constants

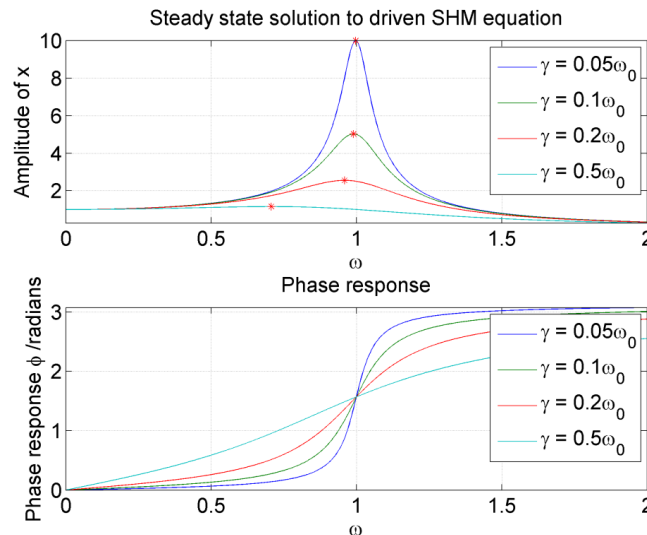
$$X(t) = \begin{cases} \text{'Critically damped'} \\ e^{-\gamma t} (A_1 + A_2 t) & \gamma = \omega_0 \\ \text{'Overdamped'} \\ e^{-\gamma t} (A_1 e^{t\sqrt{\gamma^2 - \omega_0^2}} + A_2 e^{-t\sqrt{\gamma^2 - \omega_0^2}}) & \gamma > \omega_0 \\ \text{'Underdamped - i.e. oscillatory' *} \\ Ae^{-\gamma t} \cos(t\sqrt{\omega_0^2 - \gamma^2} - \Phi) & \gamma < \omega_0 \end{cases}$$

We already know:

$$Y(t) = B \sin(\omega t - \phi) \quad B = \frac{A_0 \omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2 \omega^2}}$$

$$\phi = \tan^{-1} \left( \frac{2\gamma\omega}{\omega_0^2 - \omega^2} \right) \quad B_{\max} \text{ when } \omega = \sqrt{\omega_0^2 - 2\gamma^2}$$

$$B_{\max} = \frac{A_0 \omega_0^2}{2\gamma \sqrt{\omega_0^2 - \gamma^2}}$$



If we consider only the *oscillatory* solutions:

$$\frac{d^2x}{dt^2} + 2\gamma \frac{dx}{dt} + \omega_0^2 x = A_0 \omega_0^2 \sin \omega t$$

$$\gamma < \omega_0$$

$$x(t) = Ae^{-\gamma t} \cos(t\sqrt{\omega_0^2 - \gamma^2} - \Phi) + B \sin(\omega t - \phi)$$

$$B = \frac{A_0 \omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2 \omega^2}}$$

$$\phi = \tan^{-1} \left( \frac{2\gamma\omega}{\omega_0^2 - \omega^2} \right)$$

Let us constrain this further by considering initial conditions

$$x(0) = x_0, \quad \left. \frac{dx}{dt} \right|_{t=0} = \dot{x}_0$$

$$x_0 = A \cos(-\Phi) + B \sin(-\phi)$$

$$x_0 = A \cos \Phi - B \sin(\phi)$$

$$x_0 + B \sin \phi = A \cos \Phi$$

Noting even and odd properties of sine and cosine

$$\frac{dx}{dt} = -\gamma Ae^{-\gamma t} \cos(t\sqrt{\omega_0^2 - \gamma^2} - \Phi) + \dots$$

$$-Ae^{-\gamma t} \sqrt{\omega_0^2 - \gamma^2} \sin(t\sqrt{\omega_0^2 - \gamma^2} - \Phi) + B\omega \cos(\omega t - \phi)$$

$$\left. \frac{dx}{dt} \right|_{t=0} = -\gamma A \cos(-\Phi) + \dots$$

$$-A\sqrt{\omega_0^2 - \gamma^2} \sin(-\Phi) + B\omega \cos(-\phi)$$

$$\dot{x}_0 = -\gamma A \cos \Phi + A\sqrt{\omega_0^2 - \gamma^2} \sin \Phi + B\omega \cos \phi$$

\*Note  $\cos \theta = \frac{1}{2}(e^{i\theta} + e^{-i\theta})$ ,  $\sin \theta = \frac{1}{2i}(e^{i\theta} - e^{-i\theta})$

$$\dot{x}_0 = -\gamma(x_0 + B \sin \phi) + \frac{x_0 + B \sin \phi}{\cos \Phi} \sqrt{\omega_0^2 - \gamma^2} \sin \Phi + B\omega \cos \phi$$

$$\dot{x}_0 = -\gamma(x_0 + B \sin \phi) + (x_0 + B \sin \phi) \sqrt{\omega_0^2 - \gamma^2} \tan \Phi + B\omega \cos \phi$$

$$\frac{\dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi}{(x_0 + B \sin \phi) \sqrt{\omega_0^2 - \gamma^2}} = \tan \Phi$$

$$\frac{x_0 + B \sin \phi}{\cos \Phi} = A$$

Now let us consider similar initial conditions for **critical damping**:

$$\gamma = \omega_0$$

$$x(t) = e^{-\gamma t} (A_1 + A_2 t) + B \sin(\omega t - \phi)$$

$$B = \frac{A_0 \omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2 \omega^2}}$$

$$\phi = \tan^{-1} \left( \frac{2\gamma\omega}{\omega_0^2 - \omega^2} \right)$$

Notice the linear dependence on  $t$  is necessary to make this work

$$A_1 = x_0 + B \sin \phi$$

$$A_2 = \dot{x}_0 + \gamma A_1 - B\omega \cos \phi$$

$$A_2 = \dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi$$

$$x(0) = x_0, \quad \left. \frac{dx}{dt} \right|_{t=0} = \dot{x}_0$$

$$x_0 = A_1 - B \sin \phi$$

$$\frac{dx}{dt} = e^{-\gamma t} (A_2) - \gamma e^{-\gamma t} (A_1 + A_2 t) + B\omega \cos(\omega t - \phi)$$

$$\dot{x}_0 = A_2 - \gamma A_1 + B\omega \cos \phi$$

Finally, let us consider the **over-damped** solutions:

$$\gamma > \omega_0$$

$$x(t) = e^{-\gamma t} \left( A_1 e^{t\sqrt{\gamma^2 - \omega_0^2}} + A_2 e^{-t\sqrt{\gamma^2 - \omega_0^2}} \right) + B \sin(\omega t - \phi)$$

$$B = \frac{A_0 \omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2 \omega^2}}$$

$$\phi = \tan^{-1} \left( \frac{2\gamma\omega}{\omega_0^2 - \omega^2} \right)$$

$$x(0) = x_0, \quad \left. \frac{dx}{dt} \right|_{t=0} = \dot{x}_0$$

$$x_0 = A_1 + A_2 - B \sin \phi \quad \therefore A_1 + A_2 = x_0 + B \sin \phi$$

$$\frac{dx}{dt} = e^{-\gamma t} \sqrt{\gamma^2 - \omega_0^2} \left( A_1 e^{t\sqrt{\gamma^2 - \omega_0^2}} - A_2 e^{-t\sqrt{\gamma^2 - \omega_0^2}} \right) + \dots$$

$$-\gamma e^{-\gamma t} \left( A_1 e^{t\sqrt{\gamma^2 - \omega_0^2}} + A_2 e^{-t\sqrt{\gamma^2 - \omega_0^2}} \right) + B\omega \cos(\omega t - \phi)$$

$$\dot{x}_0 = \sqrt{\gamma^2 - \omega_0^2} (A_1 - A_2) - \gamma (A_1 + A_2) + B\omega \cos \phi$$

$$\frac{\dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi}{\sqrt{\gamma^2 - \omega_0^2}} = A_1 - A_2$$

$$\therefore 2A_1 = x_0 + B \sin \phi + \frac{\dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi}{\sqrt{\gamma^2 - \omega_0^2}}$$

$$A_1 = \frac{1}{2} (x_0 + B \sin \phi) + \frac{\dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi}{2\sqrt{\gamma^2 - \omega_0^2}}$$

$$A_2 = \frac{1}{2} (x_0 + B \sin \phi) - \frac{\dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi}{2\sqrt{\gamma^2 - \omega_0^2}}$$

## SHM in summary

$$\frac{d^2x}{dt^2} + 2\gamma \frac{dx}{dt} + \omega_0^2 x = A_0 \omega^2 \sin \omega t$$

$$x(0) = x_0, \quad \left. \frac{dx}{dt} \right|_{t=0} = \dot{x}_0$$

'Transient'

### Under-damped - oscillatory

$$\gamma < \omega_0$$

$$x(t) = Ae^{-\gamma t} \cos\left(t\sqrt{\omega_0^2 - \gamma^2} - \Phi\right) + B \sin(\omega t - \phi)$$

$$\Phi = \tan^{-1} \left( \frac{\dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi}{(x_0 + B \sin \phi)\sqrt{\omega_0^2 - \gamma^2}} \right)$$

$$A = \frac{x_0 + B \sin \phi}{\cos \Phi}$$

$$B = \frac{A_0 \omega_0^2}{\sqrt{(\omega_0^2 - \omega^2)^2 + 4\gamma^2 \omega^2}}$$

$$\phi = \tan^{-1} \left( \frac{2\gamma\omega}{\omega_0^2 - \omega^2} \right)$$

'Steady state' solution amplitude and phase

### Critically damped

$$\gamma = \omega_0$$

$$x(t) = e^{-\gamma t} (A_1 + A_2 t) + B \sin(\omega t - \phi)$$

$$A_1 = x_0 + B \sin \phi$$

$$A_2 = \dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi$$

$$B_{\max} \text{ when } \omega = \sqrt{\omega_0^2 - 2\gamma^2}$$

$$B_{\max} = \frac{A_0 \omega_0^2}{2\gamma \sqrt{\omega_0^2 - \gamma^2}}$$

Note we only get a resonance peak when

$$\omega_0^2 - 2\gamma^2 \geq 0$$

$$\gamma \leq \frac{\omega_0}{\sqrt{2}}$$

$$\gamma \leq 0.7011\omega_0$$

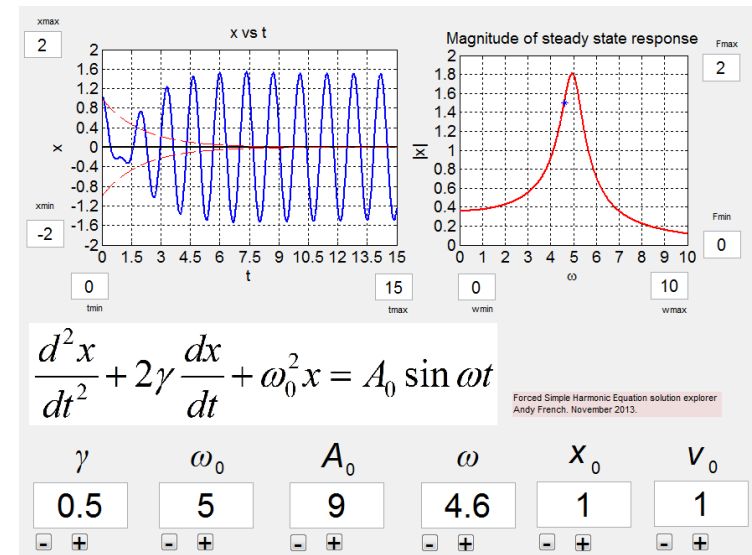
### Over-damped

$$\gamma > \omega_0$$

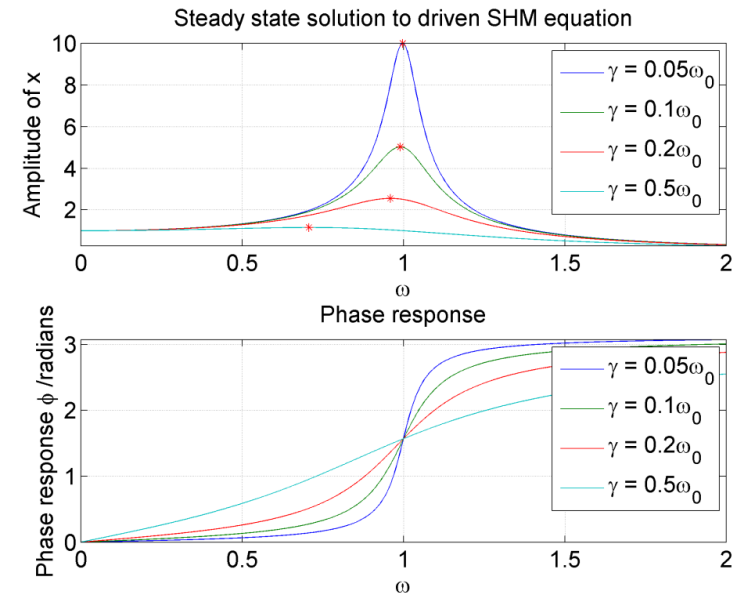
$$x(t) = e^{-\gamma t} \left( A_1 e^{t\sqrt{\gamma^2 - \omega_0^2}} + A_2 e^{-t\sqrt{\gamma^2 - \omega_0^2}} \right) + B \sin(\omega t - \phi)$$

$$A_1 = \frac{1}{2} (x_0 + B \sin \phi) + \frac{\dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi}{2\sqrt{\gamma^2 - \omega_0^2}}$$

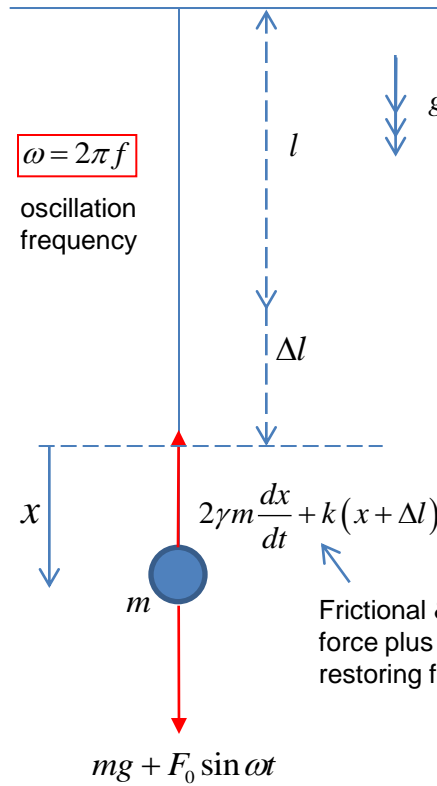
$$A_2 = \frac{1}{2} (x_0 + B \sin \phi) - \frac{\dot{x}_0 + \gamma(x_0 + B \sin \phi) - B\omega \cos \phi}{2\sqrt{\gamma^2 - \omega_0^2}}$$



Note this resonance frequency will always be less than or equal to the natural frequency



### Example system #1: Mass, spring system



$$g = 9.81 \text{ ms}^{-2}$$

By Newton's Second Law:

$$m \frac{d^2 x}{dt^2} = mg + F_0 \sin \omega t - 2\gamma m \frac{dx}{dt} - k(x + \Delta l)$$

At equilibrium  $x = 0$ ,  $F_0 = 0$

$$0 = mg - k\Delta l \quad \therefore \Delta l = \frac{mg}{k}$$

$$2\gamma m \frac{dx}{dt} + k(x + \Delta l)$$

Frictional &/or low speed drag force plus Hookean spring restoring force model

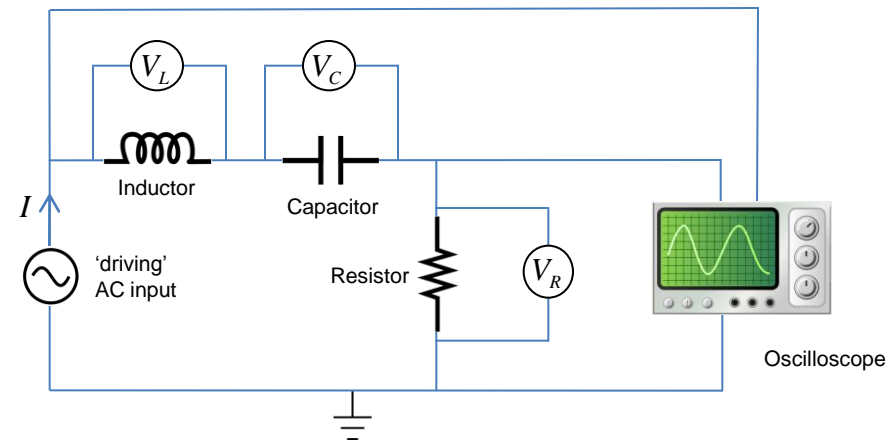
$$mg + F_0 \sin \omega t$$

Hence:  $m \frac{d^2 x}{dt^2} + 2\gamma m \frac{dx}{dt} + kx = F_0 \sin \omega t$

$$\frac{d^2 x}{dt^2} + 2\gamma \frac{dx}{dt} + \omega_0^2 x = A_0 \omega_0^2 \sin \omega t$$

$$\omega_0 = \frac{k}{m}, \quad A_0 \omega_0^2 = \frac{F_0}{m}$$

### Example system #2: R,L,C electrical circuit



Let current  $I$  flow through the circuit above. The net EMF  $V - V_L$  must equal the sum of the potential drops across each electrical component.

$$V_R + V_C = V - V_L$$

$$V_R = IR$$

$$Q = CV$$

$$V_C = \frac{1}{C} \int Idt \quad \leftarrow \quad I = \frac{dQ}{dt} \quad \therefore CV = \int Idt$$

$V_L$  is the 'back EMF' due to induction in the inductor coil

$$V_L = L \frac{dI}{dt}$$

Consider an oscillatory driving voltage  $V = V_0 \cos \omega t$

$$\frac{dV_R}{dt} + \frac{dV_C}{dt} + \frac{dV_L}{dt} = \frac{dV}{dt}$$

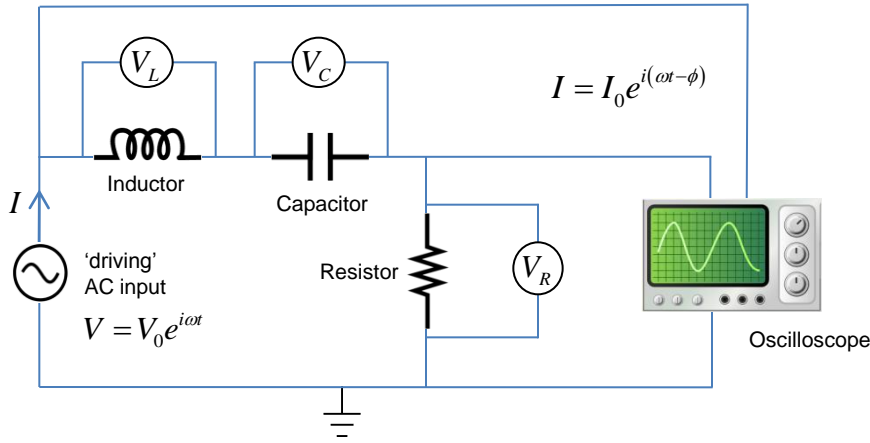
$$L \frac{d^2 I}{dt^2} + R \frac{dI}{dt} + \frac{1}{C} I = -\omega V_0 \sin \omega t$$

$$\frac{d^2 I}{dt^2} + \frac{R}{L} \frac{dI}{dt} + \frac{1}{LC} I = \frac{-\omega V_0}{L} \sin \omega t \quad \text{i.e. equation of forced SHM in } I(t)$$

$$\gamma = \frac{R}{2L}, \quad \omega_0^2 = \frac{1}{LC}, \quad A_0 \omega_0^2 = \frac{-\omega V_0}{L}, \quad x = I$$

$$\frac{d^2 x}{dt^2} + 2\gamma \frac{dx}{dt} + \omega_0^2 x = A_0 \omega_0^2 \sin \omega t$$

### Example system #3: R,L,C electrical circuit – using complex impedances



$$V_R + V_C = V - V_L$$

$$V_R = IR$$

$$V_C = \frac{1}{C} \int Idt \quad \leftarrow Q = CV$$

$$V_L = L \frac{dI}{dt}$$

$$IR + \frac{1}{C} \int Idt + L \frac{dI}{dt} = V_0 e^{i\omega t}$$

$$I = \frac{dQ}{dt} \therefore CV = \int Idt$$

$$IR + \frac{1}{C} \int Idt + L \frac{dI}{dt} = V_0 e^{i\omega t}$$

$$I_0 e^{i(\omega t - \phi)} \left( R + \frac{1}{i\omega C} + i\omega L \right) = V_0 e^{i\omega t}$$

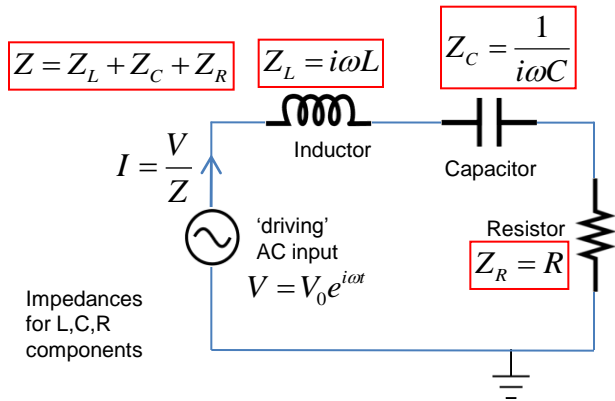
$$Z = R + \frac{1}{i\omega C} + i\omega L$$

$$\therefore V = I |Z| e^{i \arg(Z)}$$

$$\phi = \arg(Z)$$

$$\therefore V = IZ$$

Ohm's Law, generalized for AC



$$\frac{V_{out}}{V_{in}} = \frac{Z_R}{Z_L + Z_C + Z_R}$$

$$\frac{V_{out}}{V_{in}} = \frac{R}{R + i \left( \omega L - \frac{1}{\omega C} \right)}$$

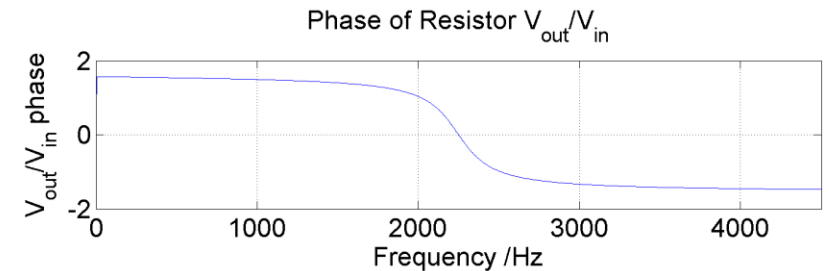
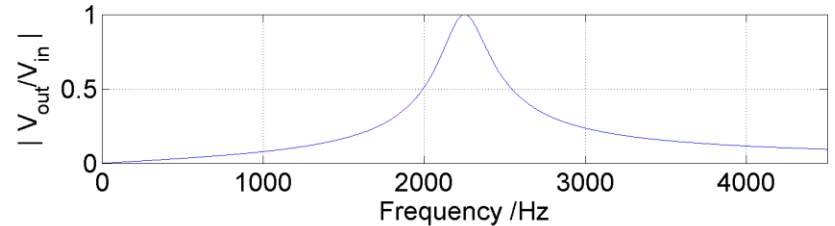
$$\frac{V_{out}}{V_{in}} = \frac{RC\omega}{RC\omega + i(\omega^2 LC - 1)}$$

$$\frac{V_{out}}{V_{in}} = \frac{2\pi f\tau}{2\pi f\tau + i \left( \frac{4\pi^2 f^2}{4\pi^2 f_0^2} - 1 \right)}$$

$$\frac{V_{out}}{V_{in}} = \frac{2\pi x f_0 \tau}{2\pi x f_0 \tau + i(x^2 - 1)}$$

$$\frac{V_{out}}{V_{in}} = \frac{2\pi x\alpha}{2\pi x\alpha + i(x^2 - 1)}$$

Magnitude of Resistor  $V_{out}/V_{in}$   
 $f_0 = 2250.7908 \text{ Hz}$ ,  $f_{max} = 2228.1692 \text{ Hz}$ ,  $RC = 1e-005 \text{ s}$ ,  $\alpha = 0.022508$   
 $L = 0.5 \text{ H}$ ,  $C = 1e-008 \text{ F}$ ,  $R = 1000 \text{ ohms}$



Note is you want a voltage gain in resonance swap over the resistor and the capacitor in the circuit above

$$x = \frac{f}{f_0} \quad f_0 = \frac{1}{2\pi} \sqrt{\frac{1}{LC}}$$

$$\tau = RC \quad \alpha = f_0 \tau$$

Characteristic time and frequency parameters for the RCL circuit